

SAVE-ON-SEPTIC SERVICES INC



Wild Rose Garden Centre 750 Tin Can Alley Gabriola Island, B.C.

October 12, 2023

Project Reference: Feasibility study and Assessment of site conditions on Lot B, Plan 60373 for suitability for development of a wastewater treatment and dispersal system- 750 Tin Can Alley, Gabriola Island, B.C.

Attn: Kent Moen,

Background:

Mr. Kent Moen (owner) is proposing a residential/commercial mixed-use development for retail and food services on Lot B, located at 750 Tin Can Alley near the village. This report will provide information on the feasibility of providing an on-site wastewater treatment and dispersal system for this project. I will provide the soils testing data and a conceptual design of the wastewater treatment and dispersal system that will meet or exceed the requirements of the Standards of Practice Manual (SPM). I will outline our approach to minimize the environmental impact on the site.

Scope of Work:

The soil investigation involved digging 1.2m deep test pits with a machine to determine the soil characteristics and ability to renovate wastewater. I was also investigating the winter water table depths and surface features such as storm water run-off impact, proximity to a drinking water source and property boundaries. There appears to be a layer of solid rock at various depths that tends to slope in a southerly direction towards North Road. There is a drinking water well 100 meters south of the test area and we would need to minimize the impact on this potable water source. 10 test pits were dug and logged for characteristics and are included in this report. To test the permeability of the soils 4 test holes were dug and perk tests performed to document the suitability of the soil to renovate wastewater. The site conditions and soils will meet the strict guidelines set out in the SPM to minimize any environmental impact. This report also reviews the various options for pre-treatment and discuss the most appropriate level of treatment prior to dispersal.

Site Evaluation:

The property tends to slope towards the southwest corner at an overall slope of 7-8% and the upper half having a gentler slope about 5%. The site has had impact from tree removal and vehicle traffic from the garden centre. The soils in the test area located neat the northern boundary appears to be less impacted by development.

I saw no evidence of stormwater erosion or impact from stormwater runoff and the site appears to be well drained. According to regional maps the principal soil type is a well drained Saturna soil. The location of the well was situated about 100 meters downslope along the eastern boundary. No other neighboring wells were encountered during this investigation. This well exceeds the setback distance (30m) and should pose no environmental impact from the dispersal area. There was a large outcrop of bedrock encountered in several locations that limit the area for dispersal, however the design shall take this into consideration to avoid discharging into these areas where thin soils are present. Both the dispersal area and the receiving area shall have sufficient depths of soil to adequately renovate the wastewater discharge to mitigate the environmental impact on the site. The northern neighbouring property has a pipe discharging stormwater onto the site and into a rock pit. This rock pit will be diverted to a new location that does not impact the dispersal site.

Test Pits:

There are a total of 10 test pits that were machine dug to a depth of about 1.2m or less if a limiting layer was encountered. There were 2 that were too shallow due to solid rock near the surface (see sketch) and were mapped as an area to avoid for development. The remaining 8 test pits revealing the stratified layer and soil types were documented. (See attached soil Logs) These test pits were then compared with the SPM requirements and other factors such as root penetration into the soils as well as soil mottling indicating the presence of the winter watertable. The results of this testing determined that there was 64cm-112cm of permeable soil overlaying a restrictive layer such as solid sandstone rock or winter watertable. The SPM requires a minimum separation of 60 cm for type 1,2&3 effluent discharges. We have sufficient depth for all 3 types with a sand filled bed design per the SPM. There is sufficient area to support a type 1 drain field design. Based on calculated daily flows of 9095L per day and soil permeability the required field length would need to be approximately 250m (820 feet) in total with a minimum length per run of 27.6m (90.6 feet) to meet the linear loading requirements of the SPM.

Percolation Testing:

There were 3 percolation tests performed on the site within the test area. (see attached test results) This test determines the ability of the soil to effectively move downward through the soil to renovate the wastewater prior to coming into contact with the under-laying ground water. The more porous the soils allow the wastewater to move quickly down through the soil. In our case the soils proved to be in the class of coarse sand and has a very high permeability. This class of soils allows the wastewater to move through the soil particles to quickly thus only partially treating the wastewater. In order to overcome this we need to pressure dose the field and limit the amount of effluent per dose (micro-dosing) using a timer in the control panel. This will allow the wastewater to be held between the soil particles by osmosis allowing it to come into contact with the micro-organisms for a longer duration thus providing better treatment of the wastewater prior to reaching the limiting layer. For coarse textured soils the hydraulic loading rate would be 40L/m2/day.

Percolation Results:

PH #1- Average 1:50 mins. /inch PH #2- Average 2:00 mins. /inch PH #3- Average 1:15 mins. /inch

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Coarse Sandy Soils:

The soil log results indicate that the characteristics of the permeable layer encountered on site are predominantly coarse sand with 10-15% cobbles. This has a loading rate in the SPM of 40L/m2/day for Type 1 discharges. These soils are very well drained and with certain design considerations are capable of effectively removing contaminants from the wastewater. These design considerations are pressure dosing and timed dosing per the SPM.

Daily Design Peak Flows:

The estimated flows generated from the proposed development are as follows:

-60 Seat restaurant- 60X90L/person -5400L (Phase 2)

-Retail garden centre and 1 bedroom residential- Retail- 139m2 x 5L= 695L

Apartment- 600L

-Coffee shop/Bakery

120persons x 20L= 2400L

TOTAL 9095L per day

Characteristics of the Wastewater:

The retail space and residential suite are both considered to be residential strength wastewater. The coffee shop and restaurant are considered to discharge high strength wastewater. This high strength component in the wastewater discharge would be required to be pre-treated to reduce both the FOG (Fats Oils & Grease) and the high BOD/TSS from the waste stream prior to discharging into the drain field (Must meet Type 1 treatment levels). This involves providing grease interceptor tanks and type 2 aeration and settling to reduce it to acceptable levels. An engineer is required to have oversight in the design of this high strength treatment system per the SPM.

Area for Drain Field:

The area of infiltrative surface requirements for Type 1 effluent discharge is as follows:

$$AIS = \frac{9095L}{40} = \frac{227.38 \text{ m}}{2}$$

Total Length of Field= 227.38m2 = 249.87 Lineal Metres (820 lineal feet) 0.91m (Maximum Width of Trench per SPM)

Linear Loading Length = 9095L = 27.56m (This is the minimum length of trench per SPM)

The drain field laterals would be 96 feet long and center fed from a central 2" Dia. manifold. There would be 9 laterals evenly spaced at 6 feet on centre. The area required for the drain field would need to be 100 feet long by 54 feet wide and be positioned perpendicular to the slope. The position of the drain field would have to meet all setback requirements of the SPM. The test area would be large enough to accommodate this field design. There is also an area eastern boundary that is large enough and could be developed for a 50% reserve area should problems arise.

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Local Area Water Wells:

There is only one well within close proximity of the wastewater system. This drilled well services our site (Lot B) and is located downslope approximately 100m away from the proposed drain field test site. The Lot above (Lot C) is served by a rainwater catchment system with a cistern tank. The location of the only well in the area exceeds the 30m setback requirements of the SPM.

Appropriate Design Considerations:

- -All components of the wastewater system meet or exceed the requirements of the SPM.
- -Providing the appropriate level of treatment for the high strength component the project and engaging an engineer to review the proposed design per the SPM.
- -Provide redundancy in the system to reduce the risk of untreated wastewater discharges on the

Conclusion:

Lot B at 750 Tin Can Alley has sufficient potential to disperse pre-treated wastewater in the ground safely without any degradation of the local environment or contamination of the local drinking water source that under-lays the site. All of the setback and regulatory requirements within the SPM can be met by the designer. Since the high strength wastewater is being proposed for this development a review of the design is required and all documents must be stamped by a professional engineer prior to submission to Vancouver Island Health Authority.

Proposed Design Options:

The residential/ retail portion of the discharge can be Type 1 treatment prior to dispersal. The high strength portion of the discharge must undergo further treatment to reduce the wastewater strength to meet or exceed Type 1 treatment levels. This wastewater must have reductions of FOG (Fat, Oils & Grease) and BOD/TSS to 20mgL FOG/ 300 BOD/ 250 TSS to be able to safely be dispersed in the drain field without degradation to the receiving environment.

Environmental Impact:

Once discharges start the pre-treatment tanks and treatment devises will provide a wastewater discharge suitable to be dispersed into the ground. Once dispersed into the soils natural processes will complete the full renovation of the wastewater. The risk to the environment shall be eliminated by choosing the most effective pre-treatment devices to reduce the wastewater to Type 1 treatment levels prior to discharge.

Operation & Maintenance:

The SPM dictates that on-going maintenance must be performed on all septic systems to ensure proper operating levels are met. The bi-annual maintenance must be performed by a qualified service provider (ROWP). To ensure proper levels of treatment are being met it would be recommended that testing of the wastewater be performed annually. An Operations and Maintenance manual will be provided to the owner by the designer per the SPM.

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If you have any questions, please contact me at 250-748-5676

Kind Regards,

Steve Brydges, ROWP Save On Septic Services Inc.



Email: saveonseptic@shaw.ca

SEE SKETCH PLAN FOR LOCATIONS.

Observed Soil Conditions

Test Pit Logs

Dot	0*- /	2-	/ 0%						***************************************
Dat	e . S	EPT. 21/	23 Site: 7	750 Tim	CAN A	LEY	Logged b	y: Mike	5DB
TP#	# 1	Pit Loc	Site: -	. END O	FD/FIEL	DSITE	Slope	\$ 6-	7%
			Soil Hori	zons (depth	s measured i	in cm/m/in	1/tt)		
Depth from to		Colour	Texture	Structure	Rupture resistance (or density)	Coarse gravel (%)	Roots depth & quantity	Mottles depth & quantity	Moisture seepage
0		Brown	Topsoi/	56.	loose	1%	YES	NB	1/25
1"		4. Brown	S. Loam	56	1000C	5%	YES	Ø	15
11"			C. Sand.	56.	10050	10-15%	YES	Ø	B
35	1/4	Tan	Clay Bell	- massive	hard	5%	MO	yes	Ø
			,	Roots	to 35"	/w/re	35"		
	2 pth	Pit Location: 4	EAST OF Texture	ア ル # /・ Structure	Slope: 7- 8 Rupture resistance	Coarse gravel	Roots depth &	Mottles depth &	Moisture
from					(or density)	(%)	quantity	quantity	seepage
0			TOPSOIL J		LOSSE	2%	YES	NO	No
51	25"		S. LOAM		1005E	5%	YES	Ø	Ø
254		SOUD S	ANDSTON	E ROCK		DO NA	YES	8	18
				Roots +	27511	11/2	ot prese	n of	
				1	~~	91 1	or prese	AL	
Note	es								

Based on USDA Field Book for Describing and Sampling Soils (2002).



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Observed Soil Conditions

Test Pit Logs

Dat	e*:	SEPT. 21/	23 Site:	750 TIN	CAN AL	LEY.	Logged b	y: Mike <	SDIS
TP#	ŧ :	3 Pit Loc	23 Site: ation: 50	WOFEA	ST-BOUND	ARY -		:88 8ch	
		****	Soil Hori	zons (depth	s measured i	n cm/m/in			
De from	to	Colour	Texture	Structure	Rupture resistance (or density)	Coarse gravel (%)	Roots depth & quantity	Mottles depth & quantity	Moisture seepage
0	2"	100	Topsoil	5.6.	Loose	1%	ues	6	6
2"	1	Jan !	Topsoil C. Sand.	5.G.	1	5-10%	yes	05	100
26	7	SOLID	SANDST	ONE RO	CK @ 26	n	/ -		1.
			Root	s to 20	" No	W/T.			
Note									
INOLO	35								
TP#	4	Pit Location:	W. of E. H	210'	Slope: 6-7				
De	pth	Pit Location:	W. of E. H.	Ž 10 ' Structure	Slope: 6-7 Rupture resistance (or density)	Coarse gravel (%)	Roots depth & quantity	Mottles depth & quantity	Moisture seepage
De	pth	and a second	Texture Topsoil	Structure SG.	Rupture resistance	Coarse gravel	depth & quantity	depth &	
De	to	BROWN Brown	Texture Topsoil C:Sand	Structure SG. S.G.	Rupture resistance (or density) Loose Loose	Coarse gravel (%)	depth &	depth & quantity	seepage
De from	to	Colour	Texture Topsoil C:Sand	Structure SG.	Rupture resistance (or density) Loose Loose	Coarse gravel (%)	depth & quantity	depth & quantity	seepage
De from	to	BROWN Brown	Texture Topsoil C:Sand	Structure SG. S.G.	Rupture resistance (or density) Loose Loose	Coarse gravel (%)	depth & quantity	depth & quantity	seepage
De from	to	BROWN Brown	Texture Topsoil C:Sand	Structure SG. S.G.	Rupture resistance (or density) Loose Loose	Coarse gravel (%)	depth & quantity	depth & quantity	seepage
De from	to	BROWN Brown	Texture Topsoil C:Sand	Structure SG. S.G.	Rupture resistance (or density) Loose Loose	Coarse gravel (%)	depth & quantity	depth & quantity	seepage
De from	to 3"	BROWN Brown	Texture Topsoil C:Sand	Structure SG. S.G.	Rupture resistance (or density) Loose Loose	Coarse gravel (%)	depth & quantity	depth & quantity	seepage
from D 3	to 3"	BROWN Brown	Texture Topsoil C:Sand	Structure SG. S.G.	Rupture resistance (or density) Loose Loose	Coarse gravel (%)	depth & quantity	depth & quantity	seepage

Based on USDA Field Book for Describing and Sampling Soils (2002).

* Date water table measured

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Observed Soil Conditions

Test Pit Logs

Dat	e*: <	EPT 21/2	3 Site:	750-111	Calxus		l onned h	W. MHZ	<i></i>
TP±	<u> </u>	7 Dit Loo	ection: al A	JOU INC	AN HUE	7		y: Mike <	VB_
	2	FIL LOC	allori. 9 fr	om EP	/h.		Slope	:86%	
	1		Soil Hori	zons (deptr	ns measured i	n cm/m/in	/ ft)		
De from	pth to	Colour	Texture	Structure	Rupture resistance (or density)	Coarse gravel (%)	Roots depth & quantity	Mottles depth & quantity	Moisture seepage
0	2"	Brown	Topsoil	5.G.	Loose	1%	yes	Ø	Ø
2"	34	Brown	C. Sand		41	5%	ues	do	d
34	49	Tan	Silt-Loan		"	10%	yes yes	yes	85
			Mottle	0 44" es @ 4	-11		/	/	
TP# De	oth	Pit Location: A	13' from E Texture	Structure	Rupture resistance (or density)	Coarse gravel (%)	Roots depth & quantity	Mottles depth & quantity	Moisture seepage
0	29	BROWN)	C. Sand	50.	LOOSE	5%	yes	8	Ø
29	37	" Tan	C. Sand Silt Loan	SG.	LOOSE	5-10%	B	Les	8
3	7"+	SOLID	SANDST	ONE ROC	K			7	
			Roots	to 29"	Mott	es @ 29	"		
Note	25								
		.,							

Based on USDA Field Book for Describing and Sampling Soils (2002).



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Observed Soil Conditions

Test Pit Logs

Dat	e*: ک	EPT. 21/	23 Site:	750 TIN	CAN AL	LEY	Logged b	y: Mike	THZ.
TP#	# 7	Pit Loc	ation: 491	wal E	B	/	Logged b	21-7	
			Soil Hor	rizons (depth	ns measured i	n cm/m/in	/)ft)		to
De from	pth to	Colour	Texture	Structure	Rupture resistance (or density)	Coarse gravel (%)	Roots depth & quantity	Mottles depth & quantity	Moisture seepage
0		Brown	C. Sano	15.6.	Loose		yes	B	8
14	"+	-Solid.	Sandsto	ne Roc	k				
				5 7005					
			Room	5 4014	711				
TP# Dep	oth	Pit Location:	98'W. 6	F.E. FL. Structure	Slope: 6% Rupture resistance (or density)	Coarse gravel (%)	Roots depth & quantity	Mottles depth & quantity	Moisture seepage
0	17	Brown	C. Sand Hone R	5.G.	Loose	5%	ues	0	\$
17	7	Sand	tone R	Pack			79		
				le is	100 SA	allow			
Note	es								
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Based on USDA Field Book for Describing and Sampling Soils (2002).



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Observed Soil Conditions

Test Pit Logs

Date	e*: S	EPT. 21/	23 Site:	750 TI	V CAN A	LEY	Logged b	y: Mike e	3DB
TP#		Pit Loc		87-4					
			Soil Hori	zons (depth	s measured i	n cm/m(in)			
De from	pth to	Colour	Texture	Structure	Rupture resistance (or density)	Coarse gravel (%)	Roots depth & quantity	Mottles depth & quantity	Moisture seepage
0	2"	Brown	Topsoul	56	Loose	2%	yes	Ø	Ø
2	29	Brown	C. Sernd	3G.	20050	5%	ces	Ø	8
29	37	Tan	F. Sand	,SG,	Hard.	5-10%	0	ges	Ø
37	114		Sands	tone				1	/
			00/5 60	2911/	Hottles	@29"			
Note TP# De from	oth to	Pit Location:	43'Sof	N E	Slope: 6 - Rupture resistance (or density)	8 % Coarse gravel (%)	Roots depth & quantity	Mottles depth & quantity	Moisture seepage
0	19	Brown	Topsail	56			URX	00	500
1	30	Brown	C. Sand	56			yes	0	85
30	-35	Tan	Silt	36.			1/8	yes	8
3	5+	Solid	sandot		ck,			75	
		Ko	ots 60 3	04/ M	ottles o	30"			
		.•		<i>'</i>					
Note	es	TO PROPERTY OF THE PARTY OF THE							

Based on USDA Field Book for Describing and Sampling Soils (2002).



Observed Soil Conditions

Test Pit Logs

Date	e*: <i>S</i>	EPT. 21/23	Site:	750 TIN C	AN ALLEY	·	Logged b	y:-Mike	SOB
[11		ation: 311	E. OF THE	tg			:87-8	
			Soil Hori	zons (depth	s measured ir	cm/m(in	Uft)		
De	pth to	Colour	Texture	Structure	Rupture resistance (or density)	Coarse gravel (%)	Roots depth & quantity	Mottles depth & quantity	Moisture seepage
0	2"	Brown	Topsoil	56.	Loose	2%	yes	8	8
2"	274	Brown	C. Sand	56.	Loose	10%	yes	9	Ø
27	36	Jan	F. Sand	56.	Hard	5-10%	8	yes	19
		Sold	Sandsto	re 63	6" w	nottles	@ 2711	•	
Note TP # De	2 pth	Pit Location: Colour	Texture	Structure	Slope: Rupture resistance (or density)	Coarse gravel (%)	Roots depth & quantity	Mottles depth & quantity	Moisture seepage

Based on USDA Field Book for Describing and Sampling Soils (2002). * Date water table measured

Percolation test

Location (add	dress): 750	O TIN	CAN	1411	BY	BARR	inch	File #·
Date: Sep	T. 21/23	Tested by	1: 5D1	3	2/)		, , , , , , , , , , , , , , , , , , ,	THE m.
Weather: ${\cal S}$	CUNNY							
Test number	Depth of base of hole	base of ho	nins per ir ole.	nch for wa	iter to drop	o from 6" t	to 5" from	
	from surface (cm)	#1	#2	#3	#4	#5	#6	Lowest rate (min per inch)
1	1	1:40	1:45	1:45	1:50	1:50	1:50	
2		1:50	1:50	1:45	1:56	1:55		
3		1:05	1:10	1:10	1:05	1:10	1:15	
4		1:40	1:45	1:45	1:45			
5								
6								
7								
8								
				Pero	colation rat	te for syst	em sizing	
Notes:		,	HLR	2=4	404,	Im ² /	DAY	1.





