

# STAFF REPORT

File No.: SS-RZ-2017.3

DATE OF MEETING:	July 12, 2022		
TO:	Salt Spring Island Local Trust Committee		
FROM:	Geordie Gordon, Acting Island Planner Salt Spring Island Team		
COPY:	Louisa Garbo, Acting Regional Planning Manager Salt Spring Island Team		
SUBJECT:	Rezoning for second dwelling unit. Applicant: Jamie Colligan Location: 2188 North End Rd.		

## RECOMMENDATION

# 1. That the Salt Spring Island Local Trust Committee places application SS-RZ-2017.3 in abeyance until the conclusion of the Salt Spring Island Local Trust Committee Housing Action Program Bylaw 530.

#### **REPORT SUMMARY**

This report brings forward a recommendation from staff to place the rezoning application SS-RZ-2017.3 in abeyance until the conclusion of the Housing Action Program. The applicant has indicated that they are unwilling to provide the deposit required to conduct the legal review for of the Housing Agreement (to ensure the second dwelling is rented at an affordable rate) and Section 219 Covenant (for energy efficiency requirements).

As the SS LTC is currently considering a proposed bylaw (Bylaw 530) that may affect the subject property and the lawfulness of the second dwelling, staff recommend that the proposed rezoning is put into abeyance pending the conclusion of the Housing Action Program Bylaw 530.

#### BACKGROUND

The applicant is seeking to make lawful a long-standing second dwelling that is not permitted on the subject property.

The SS LTC has considered this application on several occasions previously. The most recent consideration by the SS LTC was at their meeting of December 14, 2021, where a proposed bylaw was given first reading.

Previous staff reports can be accessed here:

## December 14, 2021:

Staff report: <a href="https://islandstrust.bc.ca/document/salt-spring-ltc-regular-meeting-agenda-4/">https://islandstrust.bc.ca/document/salt-spring-ltc-regular-meeting-agenda-4/</a> (page 300)

Meeting Minutes: <a href="https://islandstrust.bc.ca/document/salt-spring-ltc-regular-meeting-minutes-7/">https://islandstrust.bc.ca/document/salt-spring-ltc-regular-meeting-minutes-7/</a> (page 11)

## February 15, 2021:

Staff Report: <u>https://islandstrust.bc.ca/document/salt-spring-island-ltc-regular-meeting-agenda-14/</u> (page 261)

Meeting Minutes: <a href="https://islandstrust.bc.ca/document/salt-spring-ltc-regular-meeting-minutes/">https://islandstrust.bc.ca/document/salt-spring-ltc-regular-meeting-minutes/</a> (page 10)

## December 17, 2019:

Staff Report: <a href="https://islandstrust.bc.ca/document/ss-ltc-rm-agd-2019-12-17/">https://islandstrust.bc.ca/document/ss-ltc-rm-agd-2019-12-17/</a> (page 380)

Meeting Minutes: <a href="https://islandstrust.bc.ca/document/ss-ltc-rm-min-2019-12-17/">https://islandstrust.bc.ca/document/ss-ltc-rm-min-2019-12-17/</a> (page 10)

## January 29, 2019

Staff Report: <a href="https://islandstrust.bc.ca/document/ss-ltc-rm-agd-2019-01-29/">https://islandstrust.bc.ca/document/ss-ltc-rm-agd-2019-01-29/</a> (page 609)

Meeting Minutes: <a href="https://islandstrust.bc.ca/document/ss-ltc-rm-min-2019-01-29/">https://islandstrust.bc.ca/document/ss-ltc-rm-min-2019-01-29/</a> (page 15)

## ANALYSIS

## **Issues and Opportunities**

## Housing Agreement and Covenant

The rezoning application is proceeding on the basis of the applicant supplying an affordable dwelling unit with energy efficiency aspects (primarily related to appliances used in the dwelling). In order to secure these conditions of rezoning, legal review of the instruments are necessary – by Islands Trust lawyers, not the applicants'. In the absence of these instruments, it is inadvisable to move the application forward at this time.

## Housing Action Program

The SS LTC is currently considering Salt Spring Island Local Trust Committee Bylaw No. 530 to allow accessory dwelling units (ADUs) on the island -- such as the second dwelling that is the subject of this rezoning. As Bylaw 530 could impact the land use permissions of the subject property, the proposed rezoning of the subject property may be rendered unnecessary. Should Bylaw 530 receive final adoption, the secondary dwelling in question will likely only be required to go through the building permit process.

## Consultation

The proposed rezoning bylaw was referred to agencies, organizations, and Local Trust Committees listed in the staff report of December 14, 2021. A summary of responses is contained in appendix 1. An extensive reply was received from (at that time) the Ministry of Forests Lands Natural Resource Operations and Rural Development (FLNRORD) as a result of the referral of the potable water assessment report.

## First Nations

The proposed bylaw was referred to First Nations listed in the staff report of December 14, 2021. No responses to the referral were received.

## Rationale for Recommendation

The applicant has not provided the deposit necessary to move the application forward. Given the Housing Action Program work underway, staff recommend putting the subject application in abeyance until the conclusion of Bylaw 530.

## ALTERNATIVES

The SS LTC may wish to consider the following alternatives to the staff recommendation:

## 1. Deny the application

The SS LTC may deny the application. Staff advise that the implications of this alternative is file closure. If this alternative is selected, the SS LTC should state the reasons for denial. Recommended wording for the resolution is as follows:

That the Salt Spring Island Local Trust Committee proceed no further with application SS-RZ-2017.3 for the following reasons: the applicant has not provided the deposit necessary to review legal agreements required for the rezoning.

## NEXT STEPS

If the SS LTC accepts the recommended resolution, the rezoning application will be put into abeyance until the Housing Action program Bylaw 530 process is resolved.

Submitted By:	Geordie Gordon, Acting Island Planner	June 20, 2022
Concurrence:	Louisa Garbo, Acting Regional Planning Manager	June 21, 2022

## Attachments:

1. Agency, organization, and LTC referral responses summary report.



## Referrals: Bylaw SS-521

Agency	Sent	Received
BC Ambulance Services	04-Jan-2022	
Room 103:		
BC Assessment Authority	04-Jan-2022	
Policy, Audit and Legal Services: Cathie McIntyre		
BC Transit	04-Jan-2022	05-Jan-2022
520 Gorge Road East: Myrna Moore		
Comment: BC Transit is generally supportive of the rezoning. It is worth noting that the lot in		
question is not within an area currently served by transit nor does the recent Transit Future		
Service Plan (completed 2021) identify priorities to serve this area in the near future.		
Capital Regional District - All Referrals Aggie Chan and Jessica Arnet	04-Jan-2022	
625 Fisgard Street:		
Capital Regional District - SSI Senior Manager	04-Jan-2022	13-Jan-2022
145 Vesuvius Bay Road:		
Comment: Interests Unaffected.		
Cowichan Valley Regional District	04-Jan-2022	
175 Ingram Street: Mike Tippett		
Front Counter BC	04-Jan-2022	
FrontCounterBC@gov.bc.ca:		
Galiano Island Local Trust Committee	04-Jan-2022	07-Feb-2022
200 - 1627 Fort Street:		
Comment: Interests Unaffected.		
Islands Trust, Bylaw Enforcement	04-Jan-2022	
200 - 1627 Fort Street: Warren Dingman		
Mayne Island Local Trust Committee	04-Jan-2022	28-Feb-2022
Islands Trust:		
Comment: Interest Unaffected.		
Ministry of Forests, Land, Natural Resource Operations & Rural Development - Water Authorization	04-Jan-2022	
Sec		
520 Blanshard Street:		



## Referrals: Bylaw SS-521

Agency	Sent	Received
Ministry of Forests, Lands and Natural Resource Operations - Water Protection	13-Jan-2022	22-Feb-2022
# 142 - 2080A Labieux Road: Referrals Coordinator		
Comment: Please see substantive response.		
Ministry of Municipal Affairs and Housing	04-Jan-2022	
Planning and Land Use Management: Kris Nichols		
Ministry of Transportation and Infrastructure	04-Jan-2022	04-Jan-2022
Vancouver Island District Office:		
Comment: Approval Recommended for Reasons Outlined Below: The Ministry has no objections		
to this rezoning. It is suggested that the property owner apply for a secondary access permit if		
there is more than one access from the property to the road. A permit can be applied for		
through this link		
https://www2.gov.bc.ca/gov/content/transportation/funding-engagementpermits/permits		
North Pender Island Local Trust Committee	04-Jan-2022	27-Jan-2022
Islands Trust:		
Comment: Interests Unaffected.		
North Salt Spring Waterworks District	04-Jan-2022	
761 Upper Ganges Road: The Manager		
R.C.M.P.	04-Jan-2022	06-Jan-2022
401 Lower Ganges Road:		
<i>Comment:</i> The Salt Spring RCMP have no policing concerns with the proposed bylaw.		
Salt Spring Island Fire Rescue - District	04-Jan-2022	
105 Lower Ganges Road:		
Thetis Island Local Trust Committee	04-Jan-2022	
Northern Office:		
 Vancouver Island Health Authority	04-Jan-2022	
1952 Bay Street:		

x	Approval Recommended for Reasons Outlined Below
	Approval Recommended Subject to Conditions Outlined Below
	Interests Unaffected by Bylaw
	Approval Not Recommended Due to Reason Outlined Below

The Ministry has no objections to this rezoning. It is suggested that the property owner apply for a secondary access permit if there is more than one access from the property to the road.

A permit can be applied for through this link https://www2.gov.bc.ca/gov/content/transportation/funding-engagementpermits/permits

Salt Spring Island Trust Area (Island)

521

(Bylaw Number)

**Development Services Officer** (Title)

Ministry of Transportation and Infrastructure (Agency)

Haley Leech (Signature)

January 4, 2022 (Date)

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From:	Ford, Tristan <tford@bctransit.com></tford@bctransit.com>
Sent:	Wednesday, January 5, 2022 11:09 AM
То:	SSIInfo
Subject:	Salt Spring Island Proposed Bylaw No. 521 - 2188 North End Road, SSI - BC
-	Transit Response

Hi Daniela,

Thank you for providing us the opportunity to review the proposed referral.

BC Transit is generally supportive of the rezoning. It is worth noting that the lot in question is not within an area currently served by transit nor does the recent Transit Future Service Plan (completed 2021) identify priorities to serve this area in the near future.



Please let me know of any questions or concerns!

Cheers and happy New Year,

**Tristan Ford**, BASc, EIT, PMP (he / him) Transit Planner **BC Transit**  520 Gorge Road East, PO Box 9861 Victoria, BC V8W 9T5 236-969-2611 | <u>tford@bctransit.com</u> | bctransit.com

We acknowledge with respect that BC Transit delivers our mission on the ancestral territories of Indigenous Peoples across British Columbia, and their historical relationships with the land continue to this day.

From: Seabrook, Clive <Clive.Seabrook@rcmp-grc.gc.ca>
Sent: Thursday, January 6, 2022 8:17 PM
To: Daniela Murphy <dmurphy@islandstrust.bc.ca>
Subject: FW: Salt Spring Island Proposed Bylaw No. 521 - 2188 North End Road, SSI

Good evening,

Thank you for checking in with us. The Salt Spring RCMP have no policing concerns with the proposed bylaw.

Sgt. Clive Seabrook Detachment Commander Salt Spring RCMP 401 Lower Ganges Road Salt Spring Island – V8K 2V4 Phone: 250-537-5555 Fax: 250-537-1631

	Approval Recommended for Reasons Outlined Below
	Approval Recommended Subject to Conditions Outlined Below
X	Interests Unaffected by Bylaw
	Approval Not Recommended Due to Reason Outlined Below

Salt Spring Island Trust Area

(Island)

Hamphell

(Signature)

January 13, 2022

(Date)

521

(Bylaw Number)

Senior Manager SSI Electoral Area Administration

(Title)

Capital Regional District

(Agency)

	Approval Recommended for Reasons Outlined Below
	Approval Recommended Subject to Conditions Outlined Below
×	Interests Unaffected by Bylaw
	Approval Not Recommended Due to Reason Outlined Below

Salt Spring Island Trust Area

(Island)

Chank

(Signature)

January 27, 2022

521

(Bylaw Number)

Jas Chonk, Legislative Clerk

North Pender Island Local Trust Committee

	Approval Recommended for Reasons Outlined Below
	Approval Recommended Subject to Conditions Outlined Below
×	Interests Unaffected by Bylaw
	Approval Not Recommended Due to Reason Outlined Below

Salt Spring Island Trust Area

(Island)

Chank

(Signature)

521

(Bylaw Number)

Jas Chonk, Legislative Clerk

February 7-2022

Galiano Island Local Trust Committee



File: 58000-35/Salt Spring Island Bylaw 521

February 22, 2022

VIA EMAIL: ggordon@islandstrust.bc.ca

Dear Geordie Gordon,

Re: 2188 North End Rd (PID 000-276-901) on Salt Spring Island

Thank you for providing the opportunity to provide comment on the subject bylaw, pertaining to rezoning of the property at 2188 North End Rd (PID 000-276-901) on Salt Spring Island.

The property owner has submitted a hydrogeologic report, "Potable Water Assessment of Well #44431 at 2188 North End Road, SSI" prepared by Dave Gooding, P.Eng, September 2021. Islands Trust has requested that the regional hydrogeologist provide technical review of this report focussed on determination of the sustainable yield of the subject well and the likelihood of hydraulic connection between groundwater and surface water.

## Sustainable Yield

The owners of the subject 10,040 m<sup>2</sup> (2.5 acre) parcel are seeking rezoning and amendment of the Salt Spring Island Land Use Bylaw 355 (Salt Spring Island Local Trust Committee, 1999) to allow legal occupation of an accessory dwelling. Bylaw 33 requires a minimum water quantity of 1,600 litres per day per residence, equivalent to 3,200 litres per day (Table 1).

A short-term test was undertaken to verify whether the well is capable of providing a water quantity sufficient for the bylaw requirements. A 12-hour test was completed on August 5, 2021, during the summer, therefore test results are likely to represent aquifer conditions during the driest time of year. The test was completed at an average discharge rate of 3 L/min (4,320 L/d). Groundwater levels were measured manually and using a transducer within the pumping well, WTN 44431, and within an observation well on an adjacent property, WTN 46504, sited approximately 65 m to the northwest.

Annual demand (m <sup>3</sup> /y)	1,168		
	m³/d	L/min	USgpm
Minimum Daily Demand	3.20	2.2	0.6
Test pumping rate	4.32	3	0.8

*Table 1: Water requirement compared to pumping rate during the well test* 

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Ministry of Forests, Lands, West Coast Natural Natural Resource Operations Resource Region and Rural Development Water Protection Mailing Address: 2080 Labieux Rd Nanaimo, BC V9T 6J9 

 Tel:
 250 751-7220

 Fax:
 250 751-7224

 Website:
 www.gov.bc.ca/env/water

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I have independently calculated the long-term capacity using data from the first ~9 hours of the test (Table 2), with detailed calculations in Appendix A. My estimate of well capacity is lower than estimated by Gooding (2021). The methods and conclusions of my assessment are outlined below:

- a) Data from the start of pumping until 540 minutes (9 hours) into the test were utilized for analysis. The data from later in the test were not available or not usable, due to a sudden increase in well pumping rate and drawing down of the water level to below the transducer installation depth (or range of accuracy).
- b) Although not stated explicitly in the report, it is assumed that the domestic well pump remained in place in the well, and a second pump was installed, above the domestic pump, for the duration of the test which meant household use was continued during the test.
- c) Available drawdown was estimated as the depth between the static water level and the depth of the primary water-bearing fracture reported in the well construction record, consistent with common practice for assessment of water supply wells (Province of B.C., 2020). Gooding (2021) estimated the available drawdown between the static water level and the top of the well pump. However, it is not recommended to drawdown groundwater levels below the depth of the main water-bearing fracture, as this can result in fracture dewatering, turbulent groundwater flow, water oxygenation and bacterial growth that can lead to clogging of fractures and reduced well yield over time.
- d) The transducer data were not provided with the report, however the manual data for the pumping well, provided in the Appendix 3, were re-plotted for further analysis. A derivative plot (Figure 1) shows that the rate of drawdown in the well increased over time, particularly during the latter part of the test, which could be interpreted as a boundary condition such as fracture dewatering or a zone of lower permeability being encountered as the area of influence around the well expanded over the duration of pumping.
- e) The plot of drawdown over time shows two distinct slopes, one of moderate slope, and one steeper, but harder to discern due to the limited number of manual data points. The slope of observed drawdown up until 540 minutes was projected to 100-days (144,000 minutes) and to 180-days for comparison. A longer period of 180 days is more consistent with the duration of dry season in coastal B.C. during which no recharge occurs, rather than 100-days standard within the utility approval guidelines (Province of B.C., 2020).
- f) The well capacity is estimated as from 2,800 to 3,020 litres per day depending on whether the 180-day or 100-day projection of the drawdown curve is used. This would not meet the bylaw requirements of 3,200 litres per day. If the late-stage steeper part of the drawdown curve is utilized then the long-term well yield could be 1,570 litres per day, which is more consistent with water supply sufficient for zoning of one residence.
- g) The interpretation of well yield was affected by the test methodology. For example, as shown in Figure 3 below, the static water level reported at the start of the test is lower than the true non-pumping water level in the well. When the test began the groundwater levels were still in recovery from pumping for domestic water use earlier in the day. The

estimated well capacity would likely be slightly higher if the static prior to well use was used to calculate the available drawdown. Sources of error encountered during the test emphasize the importance of ensuring that groundwater levels in a well have stabilized before beginning the test and providing a secondary water supply to homeowners so that domestic pumping of the well does not create additional challenges in test interpretation.

- h) Field parameters (temperature, electrical conductivity, or total dissolved solids) were not monitored during the test, and water quality samples were not collected to verify if water is potable or requires treatment. Some forms of treatment increase water demand depending on water quality concerns and the type of treatment method used. Household water demand may be lower if water is only used for non-potable purposes, and alternate water sources are used for drinking and food preparation.
- i) It was not possible to interpret potential interference between the pumping and observation well due to the domestic use of the observation well during the test. The observation well data show cycling periods of well drawdown and recovery, with a magnitude of 40 to 50 m suggesting this well has relatively low productivity. The static water level increased in the observation well following cessation of pumping recovery of the test well, which could indicate that groundwater levels were locally depressed during the test and rebounded following the test cessation or due to recharge (e.g., from water diverted from the pumping well). The construction record for the test well (WTN 44431) reports water-bearing fractures at a depth of ~62.48 m (205 ft) below ground (bg), and compared to reported fractures in the observation well (WTN 46504) at 27.43, 70.10, 74.68 m bg (90, 230, and 245 ft bg) respectively. The non-pumping groundwater levels near the start of the test in both the pumping and observation wells are within a similar range (data were not provided to calculate the actual difference in levels). The two wells could be intersecting a similar fracture network but are likely not strongly interconnected due to overall low permeability of the rock.
- j) The subject well is constructed in Aquifer 721 (AQ721), within the Tricomali Channel groundwater management region, an area in which most properties are supplied by an individual well and septic system. Well yields in this sedimentary bedrock (sub-type 5a) aquifer are relatively low; wells in this groundwater region have a median estimated yield of 5.7 Litres/minute (1.5 USgpm), based on reported yields at the time of drilling. Groundwater levels in this area are monitored at Observation Well 438 Salt Spring Island (Ross Road), sited 5.6 km southeast of the subject well. Several neighbourhoods in the northern part of the island, especially closer to the coast, have diminished well quantity during summer months, and augment supplies with bulk water delivery (S. Cowan, personal communication, January 2022). The site is located approximately 560 m from the coast and in an area with moderately low risk of seawater intrusion (Province of B.C., 2015).
- k) Data were not provided in the well assessment report to indicate average water use in the residence and accessory dwelling for comparison to the bylaw requirements. It was also not reported if there have been any issues with the well over time. It was noted that "The tested well #44431 has been supplying water to both the residences on the subject property for over 30 years." This would suggest that the well is likely able to provide sufficient water for the residences provided onsite water use does not change significantly. The bylaw requirement for sufficient water for two residences (1,600 litres/day/residence, total 3,200 litres) is relatively high, in particular if the occupancy and facilities (e.g. number of bathrooms) in the secondary residence is less than within the primary dwelling. Average daily demand on Salt Spring Island is in the range of

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240 to 630 litres per connection, based on previous studies (Gorski & Sacré, 2019; Cowan, 2021). Due to the low permeability of the fractured rock aquifer, the area of influence around the well is likely to be small. The water has already been in use for the identified purpose since 1992 according to Islands Trust correspondence (G. Gordon, personal communication, January 13, 2022). A change in water availability in this area is not anticipated from approval of the secondary residence if the volume of use is consistent with historic rates of diversion.

Table 2: Long-term well capacity estimates

	Specific Capacity Reference				
Scenarios	m³/d	L/day	L/min	USgpm	
After 9 hours ((Q/DD <sub>time t</sub> )*Max SAD))	18.74	18,740	13.0	3.4	
Projected 100 days, drawdown to top of pump	4.22	4,200	2.9	0.8	Gooding (2021)
Projected 100 days, drawdown to Water Bearing fracture	3.02	3,020	2.1	0.6	
Projected 180 days - slope 1 (figure 2)	2.81	2,810	2.0	0.52	
Projected 180 days - slope 2 (figure 2)	1.56	1,560	1.1	0.29	

\*All calculations are inclusive of a 30% safety factor; Q means pumping rate, SAD means Safe Available Drawdown



Figure 1: First Derivative of Drawdown vs time



Figure 2: Drawdown vs time in WTN 44431 during pumping test



Figure 6: Tested well #44431 and observation well #46504 water levels btoc

Additional interpretation in GREEN for PW=Pumping well, additional interpretation in RED for OW=Observation Well

*Figure 3: Additional interpretation of pumping well and observation well response from multi-day transducer data, excerpted from Gooding (2021), Figure 6* 

Additional comments on pumping test methods and summary report:

- a) Field validation of pumping rate during the test was not reported. The test rate was given as an average (3 Litres/minute).
- b) Casing stickup above ground not reported for the test well nor for the observation well.
- c) The location of water discharge from pumping was not reported.
- d) Continuous transducer data for pumping well were not usable for later phase of pumping test. The measuring device was not installed deep enough, or groundwater level variation was out of the transducer range, resulting in flattening of the data curve from 660 to 790 minutes following the start of household use.
- e) The rate of household diversion for pumping well or for observation well during the test was not estimated nor reported, nor accounted for in the analysis.
- f) It was not reported whether the pumping well or observation well transducer data were corrected to manual measurements or for variations in barometric pressure.
- g) Water level calibration (static) and drawdown data were not reported nor provided in the report Appendix for the observation well.
- h) Field parameters (temperature, electrical conductivity, or total dissolved solids) were not monitored during the test, and water quality samples were not collected. Although this was not required by the Islands Trust bylaw, it would have been a useful additional source of data for the well owners and to improve understanding of well characteristics and suitability for potable use.
- i) The GWELLS database lists an additional well as sited on the subject parcel, WTN 81237. In the technical assessment, there was no mention of a second well on the property, therefore it is not known if it is present nor the status of its use. If a well is not in use and there is no intent to use it, to be compliant with the *Water Sustainability Act* (WSA) Section 56 and Groundwater Protection Regulation (GWPR) Part 9, the well must be decommissioned--filled throughout its depth with sealant and clean fill) by a registered qualified well driller. If there is no additional well onsite, it would be useful to know this to make a correction to the GWELLS database (Province of B.C., 2022).
- j) Although the purpose of groundwater use is considered domestic, and does not require a license, for future assessments of this type, the consulting hydrologist (engineer) is recommended to review standards and data submission requirements in the Guidance for Technical Assessments in Support of an Application for Groundwater Use in British Columbia Version 2 (Todd, et al., 2020), including the associated Table of Concordance.

## Hydraulic Connection to Surface Water

To assess potential impacts of the groundwater diversion on surface water rights and environmental flow needs for fisheries, the Islands Trust requested an evaluation of evidence for hydraulic connection between the subject well and adjacent surface water sources. Aspects related to hydraulic connection were not assessed by Gooding (2021) but were not specifically required by the Islands Trust bylaw.

The guidance document "Determining the Likelihood of Hydraulic Connection" (Province of B.C., 2016), defines hydraulic connection as being: "for the purpose of water allocation and use... the reasonable likelihood that pumping of groundwater from a well will eventually result in a change in the flow of a stream or spring or change in the level of a lake, pond, wetland that overlies or borders the aquifer, over a time period and to an extent that the decision maker must take into account in considering the environmental flow needs of the stream or whether the rights of other authorized users on the stream are likely to be detrimentally affected." Determination of the likelihood of hydraulic connection involves evaluation of subsurface geology; aquifer sub-type; presence, absence and spatial extent of low permeability confining layers (e.g., clay, till); and groundwater flow direction and elevation in comparison with stream elevation.

Surface water sources in proximity to the subject parcel and WTN 44431, include the brooks, creeks, and springs listed in Table 3 and shown in Figure 4.

Stream name	Distance from well (m)	Direction	Probability of hydraulic connection (HC) and rationale
Weisner Brook	53	southwest	Unverified stream location on subject property. Not likely HC. Vertical separation between groundwater and surface (static >15 m bgs). Brook may be local source of groundwater recharge during wet season.
Weisner Brook at PD34038 (Active)	305	southeast	Not likely HC. Vertical separation between groundwater and stream elevation. Groundwater flow direction is toward northeast.
Weisner Brook at PD34037 (Inactive)	407	northwest	Not likely HC. Vertical separation between groundwater and stream elevation. Groundwater flow direction is toward northeast.
Wellington Spring	403	north	Not likely HC. Groundwater flow direction is toward northeast, stream and groundwater table
Saunders Spring	501	east	are vertically and horizontally separated in low
Peachey Spring	525	east	permeability bedrock.
Nettles Creek	608	southeast	
Frederick Spring	700	southeast	
Kathleen Spring	841	southeast	
McFadden Creek	450	northeast	Closest distance downslope, not likely HC. Groundwater flow direction is toward McFadden Creek closer to coast. Due to low permeability of fractured bedrock aquifer and low rate of groundwater use, area of influence around the well is likely to be small (capture zone not likely to intersect creek).

Table 3: Assessment of hydraulic connection with WTN 44431 and surface streams

The closest stream, Weisner Brook is mapped as crossing the southwestern side of the subject parcel, but this location was not field verified. McFadden Creek drains an area to the east, and discharges to the coast north of the subject parcel. A series of licensed springs are also mapped southeast of the subject parcel.

Lithological records were examined for a subset of 32 wells within a 200 m buffer of Weisner Brook along its mapped extent in the non-TRIM hydrography layer (Figure 4). Depth to bedrock is shallow in this area, with an average 1.8 m (6.0 ft), ranging from no overburden (bedrock at the surface) up to a maximum overburden thickness of 6.1 m (20 ft) reported. For wells with lithological information, 74% of wells have confining materials with a median thickness of 1.7 m, described as loamy soil, red clay overlying broken sandstone or shale bedrock, while 25% of the wells in the area of the brook have limited to no overburden (lithologically unconfined conditions). Due to the limited degree of lithological confinement surface streams are a probable source of aquifer recharge. At the well there is a vertical separation between the land surface and groundwater table greater than 15 m. Groundwater elevation contours indicate that the direction of groundwater flow is generally toward the north, however hydraulic connection to McFadden Creek is not likely, due to the distance of McFadden from the well (>400 m) and relatively low permeability of the bedrock aquifer. In summary, hydraulic connection between the well and adjacent surface streams is unlikely, and adverse impacts of this domestic groundwater diversion on water availability for stream licensees and environmental flows are not anticipated.



Figure 4: Surface water sources and wells in the area of the subject parcel

## Closure

A short-term pumping test was completed to verify the ability of a domestic well to provide water for a residence and accessory dwelling on the subject property. The well has supplied water for the two residences since 1992, and a variance is being sought to bring the land use into regulatory compliance

with the Islands Trust bylaws. Based on analysis of the test results, the well capacity is estimated as from 2,800 to 3,020 litres per day, slightly lower than the bylaw requirements of 3,200 litres per day. However, considering the long-standing use, the well is likely able to provide sufficient water for the residences provided onsite water use remains in the range typical for island residences (up to 630 L/day/connection). Due to the low permeability of the fractured rock aquifer, the area of influence around the well is likely to be small, and a change in water availability for other groundwater users in this area is not anticipated from approval of the secondary residence provided the volume of use is consistent with historic rates of diversion. Hydraulic connection between the well and adjacent surface streams is unlikely, and adverse impacts of this domestic groundwater diversion on water availability for stream licensees and environmental flows are not anticipated.

An unused well on the property, if present and not intended for future use, should be decommissioned according to requirements of the *Water Sustainability Act*, Groundwater Protection Regulation.

Please let me know if you have additional questions or would like to discuss further.

Respectfully submitted,

-dioso Buinan Sylvia Barroso, MSc PGeo OLUMBIA Regional Hydrogeologist

#### Attachments: APPENDIX A – WELL CONSTRUCTION INFORMATION AND LONG-TERM CAPACITY ASSESSMENT

pc:

William Shulba wshulba@islandstrust.bc.ca

Daniela Murphy dmurphy@islandstrust.bc.ca

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#### APPENDIX A: WELL CONSTRUCTION INFORMATION AND LONG-TERM CAPACITY ASSESSMENT

LITHOLOGY

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Pumping Well Lithology (WTN 44431, 2188 North End Road, Salt Spring Island)

Depth from (ft)	Depth to (ft)	Depth from (m)	Depth to (m)	Depth from (masl)	Depth to (masl)	Material
0	5	0.00	1.52	59.00	57.48	overburden
5	100	1.52	30.48	57.48	28.52	hard sandstone shale seams
100	131	30.48	39.93	28.52	19.07	brown shale some moisture
131	205	39.93	62.48	19.07	-3.48	brown shale some moisture
205	250	62.48	76.20	-3.48	-17.20	black shale sandstone seams
250	350	76.20	106.68	-17.20	-47.68	soft black shale
350	350	106.68	106.68	-47.68	-47.68	Total depth
205 341		62.48 104.00		-3.48	59.00	WB Fracture 0.75 gpm (total estimated yield) Reported pump setting (2021 test)

SB comment - pump set below wb fracture, recommend not drawing down below fracture to avoid aeration/turbulent flow in well

	nping well (m)	65 m (north	west)							
Elevation (masl)		60		(based on WA	LLY tool)					
Static water level	1	Level (m) nr	Date 31-Oct-80							
Static water level		nr		Not reported		Approximately 16 m bgs, close in elevation so approximately same level as PW				
	- -bearing fracture (mbgs)	74.68	00 / 105 22	notreported		, approxime	1001 2011 05	<i>b) elose</i> in ele	factor so approximately same level as i	
Safety factor		0.30								
	wdown(30% safety) (est)	nc								
			-	B		Depth to		Depth to		
			Depth from (ft)	Depth to (ft) 1.5	Depth from (m) 0.00	(m) 0.46	(masl) 60.00	(masl) 59.54	Material	
			0 1.5	1.5 5	0.00	0.46 1.52	59.54	59.54 58.48	black loam sandy loam with gravel	
			5	10	1.52	3.05	58.48	56.95	brown shale	
			10	15	3.05	4.57	56.95	55.43	brown black shale	
			15	20	4.57	6.10	55.43	53.90	black shale	
			20	20	6.10	6.10	53.90	53.90	casing	
			20	90	6.10	27.43	53.90	32.57	black shale	
			90	230	27.43	70.10	32.57	-10.10	black shale	
			230	245	70.10	74.68	-10.10	-14.68	black shale	
			245	325	74.68	99.06	-14.68	-39.06	black shale	
			90 230		27.43		32.57		fracture	
					70.10		-10.10		fracture (water-bearing)	
			245		74.68		-14.68		fracture (water-bearing), total estima	ated yield
SSESSMENT OF	LONG-TERM YIELD (WTN 44431)									
Parameter			Units	Value						
Well information										
	/ell Tag Number /ell Identification Plate			44431 na						
	wner well name/number									
	/ell diameter		m	na 0.152						
	/ell radius		m	0.076						
	epth water-bearing fracture (first)		m bgs	62.48						
	epth water-bearing fracture (seco		m bgs	na						
	epth to top of aquifer	,	m bgs							
D	epth of pump (test or recommend	ed set-up)	m bgs	104.00						
Fi	nished well depth		m bgs	106.68						
A	quifer thickness (top of aquifer - w	ell bottom)	m	106.68						
Elevation informa	tion									
	round surface at well head		m asl	59	(based on WALLY	tool)				
W	/ell stickup above ground		m	nr						
E	evation water-bearing fracture (fi	rst)	m asl	-3.48						
	evation water-bearing fracture (se	econd)	m asl	nr	Single water-bear			ell log		
	epth to top of aquifer		m bgs	15.55	Static water level	(2021-08-05)	)			
	epth of pump		m asl	-45.00						
B	ottom of well		m asl	-47.68						
Vater level infor	mation (pumping well WTN 44431	.)			Date					
Sf	tatic water level (Pre-test)		m bgs	15.55	08-Aug-21					
	tatic water level (Pre-test geodetic	)	m asl	43.45	08-Aug-21					
	tatic water level (Max historic)		m bgs	nr						
	tatic water level (Max historic geo	detic)	m asl	nr						
	tatic water level (Min historic)		m bgs	nr						
R	ange static water level		m	15.55 -15.55	(	Cardia a (D.			structions for an 24 to 26 million	
	st. seasonal fluctuation in water le st. interference from adjacent well		m m	4 to 6 nr	Trom UW438 Salt	Spring (Ross	коад) 4 - 6 п	i seasonal flu	ctuation, from 21 to 26 mbgs	
Es										
Es	st. Interference from aujacent wen									
Es Es	/ater demand estimates		- /			L/min	Usgpm			
Es Es M A			m3/y m3/d	1168 3.200		L/min 2.2	Usgpm 0.6			

#### Pumping test information

	ping Test Test period	Time from	Time to	Duration	Test pumpin m <sup>3</sup> /d	L/min	Usgpm	% proposed
	Test period	Time from	Time to	(min)	m"/d	L/min	Usgpm	% proposed rate
				(11111)				Tute
	Test date 2021-08-05	9:00	21:00	720	4.3	3	1	135%
	Recovery			1047				
	Total test duration*		hours	12				
	Weighted average pumping rate		m3/d	nc				
	*Data not usable after 540 minutes	due to well us	age (increase i	n pumping rate)	- curtailed test d	duration 9 hours		
	Observation well during test							
	Well Tag Number			46503				
	Well ID			na				
	Owner							
	Distance from pumping well		m	65	Estimated fro	om map (not fiel	d verified)	
	Est. max interference from PW		m	nc				
	% SAD reduction in obs well			nc				
21 Pum	ping Test		m	14.27				
21 Pum								
1 Pum	DD after 9 hours		m	14.27	Cooding (20)	21)		
1 Pum	DD after 9 hours DD projected 100 days		m	63.45	Gooding (202	,	anual data	
<u>1 Pum</u>	DD after 9 hours DD projected 100 days DD projected 100 days - slope 1		m m	63.45 47	SB estimated	d from plot of ma		
1 Pum	DD after 9 hours DD projected 100 days DD projected 100 days - slope 1 DD projected 180 days - slope 1		m m m	63.45 47 50.5	SB estimated SB estimated	d from plot of ma d from plot of ma	anual data	
<u>1 Pum</u>	DD after 9 hours DD projected 100 days DD projected 100 days - slope 1 DD projected 180 days - slope 1 DD projected 100 days - slope 2		m m m	63.45 47 50.5 83	SB estimated SB estimated SB estimated	d from plot of ma d from plot of ma d from plot of ma	anual data anual data	
1 Pum	DD after 9 hours DD projected 100 days DD projected 100 days - slope 1 DD projected 180 days - slope 1 DD projected 100 days - slope 2 DD projected 180 days - slope 2		m m m m	63.45 47 50.5 83 91	SB estimated SB estimated SB estimated SB estimated	d from plot of ma d from plot of ma d from plot of ma d from plot of ma	anual data anual data anual data	
21 Pum	DD after 9 hours DD projected 100 days DD projected 100 days - slope 1 DD projected 180 days - slope 1 DD projected 180 days - slope 2 DD projected 180 days - slope 2 Min available drawdown		m m m m m	63.45 47 50.5 83 91 46.93	SB estimated SB estimated SB estimated SB estimated Drawdown to	d from plot of ma d from plot of ma d from plot of ma d from plot of ma o water-bearing	anual data anual data anual data fracture	ded)
21 Pum	DD after 9 hours DD projected 100 days DD projected 100 days - slope 1 DD projected 180 days - slope 1 DD projected 180 days - slope 2 DD projected 180 days - slope 2 Min available drawdown Max available drawdown		m m m m m	63.45 47 50.5 83 91 46.93 88.45	SB estimated SB estimated SB estimated SB estimated Drawdown to	d from plot of ma d from plot of ma d from plot of ma d from plot of ma	anual data anual data anual data fracture	ded)
2 <u>1 Pum</u>	DD after 9 hours DD projected 100 days DD projected 100 days - slope 1 DD projected 180 days - slope 1 DD projected 100 days - slope 2 DD projected 180 days - slope 2 Min available drawdown Max available drawdown Safety factor (%)		m m m m m m (no units)	63.45 47 50.5 83 91 46.93 88.45 0.3	SB estimated SB estimated SB estimated SB estimated Drawdown to Drawdown to	d from plot of ma d from plot of ma d from plot of ma d from plot of ma o water-bearing o top of pump (r	anual data anual data anual data fracture	ded)
<u>21 Pum</u>	DD after 9 hours DD projected 100 days DD projected 100 days - slope 1 DD projected 180 days - slope 1 DD projected 180 days - slope 2 DD projected 180 days - slope 2 Min available drawdown Max available drawdown		m m m m m	63.45 47 50.5 83 91 46.93 88.45	SB estimated SB estimated SB estimated SB estimated Drawdown to Drawdown to	d from plot of ma d from plot of ma d from plot of ma d from plot of ma o water-bearing	anual data anual data anual data fracture not recommer	
<u>21 Pum</u>	DD after 9 hours DD projected 100 days DD projected 100 days - slope 1 DD projected 180 days - slope 1 DD projected 100 days - slope 2 DD projected 180 days - slope 2 Min available drawdown Max available drawdown Safety factor (%) Min safe available drawdown (SAD) Max safe available drawdown		m m m m m (no units) m	63.45 47 50.5 83 91 46.93 88.45 0.3 32.85 61.92	SB estimated SB estimated SB estimated Drawdown tr Drawdown tr Drawdown tr	d from plot of ma d from plot of ma d from plot of ma d from plot of ma o water-bearing o top of pump (r o WB fracture o top of well pur	anual data anual data anual data fracture not recommer	
2 <u>1 Pum</u>	DD after 9 hours DD projected 100 days DD projected 100 days - slope 1 DD projected 180 days - slope 1 DD projected 180 days - slope 2 DD projected 180 days - slope 2 Min available drawdown Max available drawdown Safety factor (%) Min safe available drawdown Sapecific capacity	))	m m m m m (no units) m	63.45 47 50.5 83 91 46.93 88.45 0.3 32.85 61.92 m <sup>3</sup> /d	SB estimated SB estimated SB estimated SB estimated Drawdown tr Drawdown tr Drawdown tr Drawdown tr L/min	d from plot of ma d from plot of ma d from plot of ma d from plot of ma o water-bearing o top of pump (r o WB fracture o top of well pur Usgpm	anual data anual data anual data fracture not recommer	
<u>21 Pum</u>	DD after 9 hours DD projected 100 days DD projected 100 days - slope 1 DD projected 100 days - slope 1 DD projected 100 days - slope 2 DD projected 180 days - slope 2 Min available drawdown Max available drawdown Safety factor (%) Min safe available drawdown (SAD) Max safe available drawdown Specific capacity After 9 hours ((Q/DD <sub>time t</sub> )*Max SAD		m m m m m (no units) m	63.45 47 50.5 83 91 46.93 88.45 0.3 32.85 61.92 m <sup>3</sup> /d 18.74	SB estimated SB estimated SB estimated SB estimated Drawdown tr Drawdown tr Dr	d from plot of ma d from plot of ma d from plot of ma d from plot of ma d from plot of ma o water-bearing o top of pump (r o WB fracture o top of well pur Usgpm 3.4	anual data anual data anual data fracture not recommer	imended)
<u>21 Pum</u>	DD after 9 hours DD projected 100 days DD projected 100 days - slope 1 DD projected 180 days - slope 1 DD projected 180 days - slope 2 DD projected 180 days - slope 2 Min available drawdown Max available drawdown Safety factor (%) Min safe available drawdown (SAD) Max safe available drawdown Specific capacity After 9 hours ((Q/DD <sub>time t</sub> )*Max SAD Projected 100 days, dd to top of pur	np	m m m m m (no units) m	63.45 47 50.5 83 91 46.93 88.45 0.3 32.85 61.92 m <sup>3</sup> /d 18.74 4.22	SB estimatec SB estimatec SB estimatec SB estimatec Drawdown tr Drawdown tr Drawdown tr Drawdown tr L/min 13.0 2.9	d from plot of ma d from plot of ma d from plot of ma d from plot of ma o water-bearing o top of pump (r o WB fracture o top of well pur Usgpm 3.4 0.8	anual data anual data anual data fracture not recommer	
<u>21 Pum</u>	DD after 9 hours DD projected 100 days DD projected 100 days - slope 1 DD projected 100 days - slope 1 DD projected 100 days - slope 2 DD projected 180 days - slope 2 Min available drawdown Max available drawdown Safety factor (%) Min safe available drawdown (SAD) Max safe available drawdown Specific capacity After 9 hours ((Q/DD <sub>time t</sub> )*Max SAD	np	m m m m m (no units) m	63.45 47 50.5 83 91 46.93 88.45 0.3 32.85 61.92 m <sup>3</sup> /d 18.74	SB estimated SB estimated SB estimated SB estimated Drawdown tr Drawdown tr Dr	d from plot of ma d from plot of ma d from plot of ma d from plot of ma d from plot of ma o water-bearing o top of pump (r o WB fracture o top of well pur Usgpm 3.4	anual data anual data anual data fracture not recommer	imended)

Report reference for pumping test: "Potable Water Assessment of Well #44431 at 2188 North End Road, SSI" prepared by Dave Gooding, P.Eng, September 2021.

	Approval Recommended for Reasons Outlined Below
	Approval Recommended Subject to Conditions Outlined Below
×	Interests Unaffected by Bylaw
	Approval Not Recommended Due to Reason Outlined Below

Salt Spring Island Trust Area

(Island)

Chank

(Signature)

February 28 2022

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(Bylaw Number)

Jas Chonk, Legislative Clerk

Mayne Island Local Trust Committee